

# Grad's Moment Equations for Binary Hard Sphere Gas-Mixtures

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**Abstract** The derivation of non-linear Grad's  $2 \times 26$ -moment ( $2 \times G26$ ) equations for a binary gas-mixture of monatomic-inert-ideal hard sphere gases is sketched, although—for conciseness—only the linear  $2 \times G26$  equations are illustrated and analysed. The linear stability analysis is performed on  $2 \times G26$  equations by studying the dispersion relation and by considering the plane wave solution, it is shown that the  $2 \times G26$  equations for binary hard sphere gas-mixture are linearly stable.

**Keywords:** Moment method, Binary mixture, Kinetic theory, Knudsen number

## 1. Introduction

In the last decade, miniaturizing electronic devices has become an important focus of interest to many industries and, thus, the modelling of gas flows in micro-devices has been an intriguing problem.

As a result of shrinking down the size of devices, the mean-free-path of the gas molecules becomes comparable to the size of the device. This results into the *rarefaction* of gases inside the device. Rarefaction can be characterised by a dimensionless parameter, the Knudsen number  $Kn$ , which is defined as the ratio of mean-free-path,  $\lambda$ , of the gas molecules over a characteristic length  $L$ . The Knudsen number encountered in micro-devices often ranges from 0.01 to 1 [1] which resides in the typical range of the so-called slip flow regime ( $0.001 \lesssim Kn \lesssim 0.1$ ) and transition regime ( $0.1 \lesssim Kn \lesssim 10$ ) [2]. The processes in slip flow regime can be described using the well-known Navier–Stokes–Fourier (NSF) equations, provided they are furnished with appropriate velocity slip and temperature jump boundary conditions [3]. However, the NSF equations lose their validity in the transition regime [2, 4] and more sophisti-

cated models are needed to describe the flows in this regime.

The processes in all flow regimes can be well-described by the Boltzmann equation, which is the evolution equation for the distribution function of the gas particles. However, the direct solutions of the Boltzmann equation are computationally expensive, particularly, in the transition regime.

The approximation methods in kinetic theory offer an alternative for solving the Boltzmann equation. In kinetic theory, the two most celebrated approximation methods for solving the Boltzmann equation are *Grad's method of moments* [5–7] and the *Chapman–Enskog expansion method* [8]. Nevertheless, the equations resulting from higher-order approximation in Chapman–Enskog expansion method suffer from instability [9], hence their applicability is questionable. On the other hand, the moment equations resulting from Grad's method of moments, in case of a single gas, are always linearly stable.

Despite the success of Grad's method of moments and its variants, e.g. [4], in describing many rarefaction effects for a single gas, they have not been used enough for the mixtures, perhaps, because the pro-

duction terms—the right-hand sides resulting from the collision term in the Boltzmann equation—in the moment equations are not easy to evaluate. To the best of our knowledge, the fully non-linear Grad’s 26-moment (G26) equations for each component of a multi-temperature Maxwell gas-mixture are derived and a linear stability of Grad’s  $2 \times 26$ -moment ( $2 \times \text{G26}$ ) equations for binary gas-mixture of Maxwell gases has been analysed for the first time in [10].

Since the hard sphere molecule model is more realistic, we analyse the linear stability of  $2 \times \text{G26}$  equations for binary mixture of gases with hard sphere interaction potential in this paper. Also, it is commonly believed that the more moments one includes, the better approximation to the Boltzmann equation one obtains. That is why we chose 26 moments for each constituent in the mixture instead of 13 moments.

## 2. Boltzmann Equation

We consider a mixture of two monatomic-inert-ideal hard sphere gases  $\alpha$  and  $\beta$ . Let the molecular masses of the two gases be  $m_\alpha$  and  $m_\beta$ , and the diameters be  $d_\alpha$  and  $d_\beta$ . The state of the binary mixture of  $\alpha$  and  $\beta$  gases is characterised by the two velocity distribution functions  $f_\gamma \equiv f_\gamma(t, \mathbf{x}, \mathbf{c}_\gamma)$ ,  $\gamma \in \{\alpha, \beta\}$ , where  $\mathbf{x}$  is the position vector and  $\mathbf{c}_\gamma$  is the instantaneous velocity of the  $\gamma$ -molecule at time  $t$ . The evolutions of these distribution functions are governed by the Boltzmann equations

$$\frac{\partial f_\gamma}{\partial t} + c_i^{(\gamma)} \frac{\partial f_\gamma}{\partial x_i} + F_i^{(\gamma)} \frac{\partial f_\gamma}{\partial c_i^{(\gamma)}} = S_{\gamma\alpha} + S_{\gamma\beta} \quad (1)$$

for  $\gamma \in \{\alpha, \beta\}$ , where  $\mathbf{F}_\gamma$  is the external force per unit mass acting on  $\gamma$ -species and

$$S_{\gamma\delta} = \left( \frac{d_\gamma + d_\delta}{2} \right)^2 \int (f'_\gamma f'_\delta - f_\gamma f_\delta) |\mathbf{k}_{\gamma\delta} \cdot \mathbf{g}_{\gamma\delta}| \times \Theta(\mathbf{k}_{\gamma\delta} \cdot \mathbf{g}_{\gamma\delta}) d^2 \mathbf{k}_{\gamma\delta} d^3 \mathbf{c}_\delta \quad (2)$$

for  $\gamma, \delta \in \{\alpha, \beta\}$  are the collision terms. In (2),  $\mathbf{g}_{\gamma\delta} = \mathbf{c}_\gamma - \mathbf{c}_\delta$  is the relative velocity between two colliding molecules,  $\mathbf{k}_{\gamma\delta}$  is the unit

contact vector between the centres of two colliding molecules,  $\Theta(x)$  is the Heaviside step-function and primes are used to denote the distribution functions with post-collisional velocities  $(\mathbf{c}'_\alpha, \mathbf{c}'_\beta)$  [11], e.g.  $f'_\alpha \equiv f_\alpha(t, \mathbf{x}, \mathbf{c}'_\alpha)$ . Furthermore, the integration over velocity in (2) and in rest of the paper covers the whole velocity space  $\mathbb{R}^3$  whereas the integration over solid angle covers the unit sphere associated with the unit contact vector  $\mathbf{k}_{\gamma\delta}$ .

## 3. Moment Equations

The general form of moment of velocity distribution function  $f_\gamma$  ( $\gamma \in \{\alpha, \beta\}$ ) is

$$u_{i_1 \dots i_n}^{a(\gamma)} = m_\gamma \int C_\gamma^{2a} C_{i_1}^{(\gamma)} C_{i_2}^{(\gamma)} \dots C_{i_n}^{(\gamma)} f_\gamma d\mathbf{c}_\gamma, \quad (3)$$

where  $a, n \in \mathbb{N}_0$ ,  $\mathbf{C}_\gamma = \mathbf{c}_\gamma - \mathbf{v}$  is the peculiar velocity of  $\gamma$ -constituent with respect to the whole mixture and angular brackets around the indices denote the symmetric-traceless quantities [2];  $\mathbf{v}$  is the barycentric velocity of the mixture. The physical quantities—density  $\rho_\gamma$ , diffusion velocity  $\mathbf{u}_\gamma = \mathbf{v}_\gamma - \mathbf{v}$  (where  $\mathbf{v}_\gamma$  is the mean velocity of  $\gamma$ -component), temperature  $T_\gamma$ , stress tensor  $\boldsymbol{\sigma}_\gamma$  and heat flux  $\mathbf{q}_\gamma$  ( $\gamma \in \{\alpha, \beta\}$ )—relate with the first few moments defined by (3) as

$$\begin{aligned} \rho_\gamma &= m_\gamma n_\gamma = m_\gamma \int f_\gamma d\mathbf{c}_\gamma = u^{0(\gamma)}, \\ \rho_\gamma u_i^{(\gamma)} &= m_\gamma \int C_i^{(\gamma)} f_\gamma d\mathbf{c}_\gamma = u_i^{0(\gamma)}, \\ \frac{3}{2} \rho_\gamma \theta_\gamma &= \frac{1}{2} m_\gamma \int C_\gamma^2 f_\gamma d\mathbf{c}_\gamma = \frac{1}{2} u^{1(\gamma)}, \\ \sigma_{ij}^{(\gamma)} &= m_\gamma \int C_{(i}^{(\gamma)} C_{j)}^{(\gamma)} f_\gamma d\mathbf{c}_\gamma = u_{ij}^{0(\gamma)}, \\ q_i^{(\gamma)} &= \frac{1}{2} m_\gamma \int C_\gamma^2 C_i^{(\gamma)} f_\gamma d\mathbf{c}_\gamma = \frac{1}{2} u_i^{1(\gamma)}, \end{aligned} \quad (4)$$

where  $n_\gamma$  is the number density,  $\theta_\gamma = kT_\gamma/m_\gamma$  is the temperature in energy units, and  $k$  is the Boltzmann constant. The other higher moments defined by (3) do not represent physical quantities in general. Additionally,

the barycentric velocities of the individual components are defined as

$$\rho_\gamma v_i^{(\gamma)} = m_\gamma \int c_i^{(\gamma)} f_\gamma d\mathbf{c}_\gamma, \quad \gamma \in \{\alpha, \beta\}$$

so that the expression for momentum density of the mixture,  $(\rho_\alpha + \rho_\beta)v_i = \rho_\alpha v_i^{(\alpha)} + \rho_\beta v_i^{(\beta)}$ , implies that

$$\rho_\alpha u_i^{(\alpha)} + \rho_\beta u_i^{(\beta)} = 0. \quad (5)$$

Note that in non-equilibrium individual gases in a mixture have different temperatures [12–14], although most of the times in literature all the gases in a mixture are assumed to have a common temperature for simplicity, see e.g. [8, 11–13, 15–18]. In this paper, we consider different temperatures for different gases and, therefore, the equations presented in this paper are expected to deliver more feasible results. The total temperature of the mixture  $T$ , if required, can be evaluated using the relation for total pressure, i.e.,  $k(n_\alpha + n_\beta)T = k n_\alpha T_\alpha + k n_\beta T_\beta$ .

Moment equations for  $\gamma$ -component ( $\gamma \in \{\alpha, \beta\}$ ) in the mixture are obtained by multiplying the Boltzmann equation (1) with  $\psi_\gamma \equiv \psi(t, \mathbf{x}, \mathbf{c}_\gamma)$  and integrating over velocity space  $\mathbf{c}_\gamma$ . For 26-moment theory,  $\psi_\gamma$  is chosen from  $m_\gamma \{1, C_i^{(\gamma)}, C_\gamma^2/2, C_{(i}^{(\gamma)} C_{j)}^{(\gamma)}, C_\gamma^2 C_i^{(\gamma)}/2, C_{(i}^{(\gamma)} C_{j)}^{(\gamma)} C_k^{(\gamma)}, C_\gamma^2 C_{(i}^{(\gamma)} C_{j)}^{(\gamma)}, C_\gamma^4\}$  in order to obtain the 26-moment equations for  $\gamma$ -constituent corresponding to 26 variables  $\{n_\gamma, u_i^{(\gamma)}, T_\gamma, \sigma_{ij}^{(\gamma)}, q_i^{(\gamma)}, m_{ijk}^{(\gamma)} = u_{ijk}^{0(\gamma)}, u_{ij}^{1(\gamma)}, u^{2(\gamma)}\}$ . The  $2 \times 26$ -moment equations obtained in this way are not closed since the flux term (second term on the left-hand side) in the Boltzmann equation (1) produces the moments which are an order higher than the moments used. Additionally, the production terms in each moment equation (except the mass balance equation) are also unknown and all the moment equations contain an extra variable—the barycentric velocity of the mixture  $\mathbf{v}$ .

The system of  $2 \times 26$ -moment equations is closed by assuming Grad-type velocity distribution function for each component  $\gamma \in$

$\{\alpha, \beta\}$  based on first 26 moments of respective component:

$$\begin{aligned} f_{\gamma|G26} = f_0^{(\gamma)} & \left[ 1 + \frac{\Delta_\gamma}{8\rho_\gamma\theta_\gamma^2} \left( 1 - \frac{2C_\gamma^2}{3\theta_\gamma} + \frac{1}{15} \frac{C_\gamma^4}{\theta_\gamma^2} \right) \right. \\ & + \frac{q_i^{(\gamma)} C_i^{(\gamma)}}{5\rho_\gamma\theta_\gamma^2} \left( \frac{C_\gamma^2}{\theta_\gamma} - 5 \right) - \frac{u_i^{(\gamma)} C_i^{(\gamma)}}{2\rho_\gamma\theta_\gamma} \left( \frac{C_\gamma^2}{\theta_\gamma} - 7 \right) \\ & + \frac{\sigma_{ij}^{(\gamma)}}{2\rho_\gamma\theta_\gamma^2} C_{(i}^{(\gamma)} C_{j)}^{(\gamma)} + \frac{m_{ijk}^{(\gamma)}}{6\rho_\gamma\theta_\gamma^3} C_{(i}^{(\gamma)} C_{j)}^{(\gamma)} C_k^{(\gamma)} \\ & \left. + \left( \frac{u_{ij}^{1(\gamma)} - 7\theta_\gamma\sigma_{ij}^{(\gamma)}}{28\rho_\gamma\theta_\gamma^3} \right) C_{(i}^{(\gamma)} C_{j)}^{(\gamma)} \left( \frac{C_\gamma^2}{\theta_\gamma} - 7 \right) \right], \quad (6) \end{aligned}$$

where

$$f_0^{(\gamma)} = n_\gamma \left( \frac{1}{2\pi\theta_\gamma} \right)^{3/2} \exp \left( -\frac{C_\gamma^2}{2\theta_\gamma} \right) \quad (7)$$

is Maxwellian distribution function and  $\Delta_\gamma = u^{2(\gamma)} - 15\rho_\gamma\theta_\gamma^2$ . With this closure, the unknown higher-order moments as well as the production terms (for any interaction potential) are expressed in terms of the moments considered. For the extra variable  $\mathbf{v}$ , one needs the momentum balance equation for the mixture which may be obtained by adding the balance equations for both the diffusion velocities. Including the momentum balance equation for mixture one gets a closed system of  $(2 \times 26 + 1)$  equations. However, it is clear from (5) that the diffusion velocities of the two components in the mixture are not independent and one of them could be replaced by other using (5). Therefore, one equation for any diffusion velocity could be removed from the  $(2 \times 26 + 1)$  equations and one gets closed system of  $2 \times 26$  equations. We still refer to them as  $2 \times G26$  equations.

In principle, one can obtain the fully non-linear  $2 \times G26$  moment equations with any general interaction potential. However, evaluating the production terms for a general potential and expressing them in a nice form is not easy. Therefore, we restrict ourselves to Maxwell and hard sphere interaction potentials. The fully non-linear  $N \times G26$  equations with the production terms for Maxwell

molecules are detailed in [10] and the linear production terms for a binary gas-mixture of hard spheres are given in [19]. For better readability, we shall present only the linear  $2 \times G26$  equations for a binary gas-mixture of hard spheres with  $\mathbf{F}_\alpha = \mathbf{F}_\beta = \mathbf{0}$ .

The non-linear  $2 \times G26$  equations are linearised by perturbing the field variables around their corresponding ground states:

$$\begin{aligned} v_i &= \varepsilon \tilde{v}_i, & n_\gamma &= n_\gamma^\circ + \varepsilon \tilde{n}_\gamma, & T_\gamma &= T_\circ + \varepsilon \tilde{T}_\gamma, \\ u_i^{(\gamma)} &= \varepsilon \tilde{u}_i^{(\gamma)}, & \sigma_{ij}^{(\gamma)} &= \varepsilon \tilde{\sigma}_{ij}^{(\gamma)}, & q_i^{(\gamma)} &= \varepsilon \tilde{q}_i^{(\gamma)}, \\ m_{ijk}^{(\gamma)} &= \varepsilon \tilde{m}_{ijk}^{(\gamma)}, & u_{ij}^{1(\gamma)} &= \varepsilon \tilde{u}_{ij}^{1(\gamma)}, & \Delta_\gamma &= \varepsilon \tilde{\Delta}_\gamma, \end{aligned}$$

for  $\gamma \in \{\alpha, \beta\}$ , where  $n_\gamma^\circ$  and  $T_\circ$  are the number density of the  $\gamma$ -constituent and the common temperature, respectively, in the ground state; the ground state values of other quantities are assumed to be zero. The quantities with tilde are the corresponding perturbations from the ground state and  $\varepsilon$  is a small parameter. Next, the equations are rewritten in a dimensionless form by employing the length scale  $L$ , velocity scale  $v_0 = \sqrt{k T_\circ / m_\beta}$  for the barycentric velocity of the mixture and time scale  $t_0 = v_0 / L$ ; the number densities and temperatures are scaled with their respective ground state values and the other moments including diffusion velocities for  $\gamma$ -constituent ( $\gamma \in \{\alpha, \beta\}$ ) are scaled with appropriate powers of  $(m_\gamma n_\gamma^\circ)$  and  $(k T_\circ / m_\gamma)$ . Note that the velocity scale  $v_0$  is chosen in such a way that if one considers the gas-mixture with infinitely diluted  $\alpha$ -component, the G26 equations for  $\beta$ -constituent reduces to those for a single gas.

Here onwards, all the quantities will be in dimensionless form unless otherwise stated. The linear G26 equations for  $\alpha$ -constituent in the mixture read

$$\sqrt{r_m} \left( \frac{\partial n_\alpha}{\partial t} + \frac{\partial v_i}{\partial x_i} \right) + \frac{\partial u_i^{(\alpha)}}{\partial x_i} = 0, \quad (8)$$

$$\begin{aligned} \sqrt{r_m} \frac{\partial u_i^{(\alpha)}}{\partial t} + r_m \frac{\partial v_i}{\partial t} + \frac{\partial \sigma_{ij}^{(\alpha)}}{\partial x_j} + \frac{\partial n_\alpha}{\partial x_i} + \frac{\partial T_\alpha}{\partial x_i} \\ = -\frac{\Omega}{\text{Kn}} [\delta_1 u_i^{(\alpha)} + \delta_2 q_i^{(\alpha)} - \delta_3 u_i^{(\beta)} - \delta_4 q_i^{(\beta)}], \end{aligned} \quad (9)$$

$$\begin{aligned} \sqrt{r_m} \left( \frac{3}{2} \frac{\partial T_\alpha}{\partial t} + \frac{\partial v_i}{\partial x_i} \right) - \frac{3}{2} \frac{\partial u_i^{(\alpha)}}{\partial x_i} + \frac{\partial q_i^{(\alpha)}}{\partial x_i} \\ = -\frac{\Omega}{\text{Kn}} [\delta_5 (T_\alpha - T_\beta) + \delta_6 \Delta_\alpha - \delta_7 \Delta_\beta], \end{aligned} \quad (10)$$

$$\begin{aligned} \sqrt{r_m} \left( \frac{\partial \sigma_{ij}^{(\alpha)}}{\partial t} + 2 \frac{\partial v_{(i}}{\partial x_{j)}} \right) + \frac{\partial m_{ijk}^{(\alpha)}}{\partial x_k} + \frac{4}{5} \frac{\partial q_{(i}^{(\alpha)}}{\partial x_{j)}} \\ = -\frac{1}{28} \frac{r_n r_d^2}{\text{Kn}} [21 \sigma_{ij}^{(\alpha)} + u_{ij}^{1(\alpha)}] \\ - \frac{\Omega}{\text{Kn}} [\delta_8 \sigma_{ij}^{(\alpha)} + \delta_9 u_{ij}^{1(\alpha)} - \delta_{10} \sigma_{ij}^{(\beta)} - \delta_{11} u_{ij}^{1(\beta)}], \end{aligned} \quad (11)$$

$$\begin{aligned} \sqrt{r_m} \frac{\partial q_i^{(\alpha)}}{\partial t} + \frac{5}{2} r_m \frac{\partial v_i}{\partial t} + \frac{1}{2} \frac{\partial u_{ij}^{1(\alpha)}}{\partial x_j} + \frac{1}{6} \frac{\partial \Delta_\alpha}{\partial x_i} \\ + \frac{5}{2} \frac{\partial n_\alpha}{\partial x_i} + 5 \frac{\partial T_\alpha}{\partial x_i} = -\frac{1}{3} \frac{r_n r_d^2}{\text{Kn}} [2 q_i^{(\alpha)} - 5 u_i^{(\alpha)}] \\ - \frac{\Omega}{\text{Kn}} [\delta_{12} q_i^{(\alpha)} - \delta_{13} u_i^{(\alpha)} - \delta_{14} q_i^{(\beta)} - \delta_{15} u_i^{(\beta)}], \end{aligned} \quad (12)$$

$$\begin{aligned} \sqrt{r_m} \frac{\partial m_{ijk}^{(\alpha)}}{\partial t} + \frac{3}{7} \frac{\partial u_{ij}^{1(\alpha)}}{\partial x_k} = -\frac{3}{2} \frac{r_n r_d^2}{\text{Kn}} m_{ijk}^{(\alpha)} \\ - \frac{\Omega}{\text{Kn}} [\delta_{16} m_{ijk}^{(\alpha)} - \delta_{17} m_{ijk}^{(\beta)}], \end{aligned} \quad (13)$$

$$\begin{aligned} \sqrt{r_m} \left( \frac{\partial u_{ij}^{1(\alpha)}}{\partial t} + 14 \frac{\partial v_{(i}}{\partial x_{j)}} \right) + 9 \frac{\partial m_{ijk}^{(\alpha)}}{\partial x_k} + \frac{56}{5} \frac{\partial q_{(i}^{(\alpha)}}{\partial x_{j)}} \\ - 14 \frac{\partial u_{(i}^{(\alpha)}}{\partial x_{j)}} = -\frac{1}{168} \frac{r_n r_d^2}{\text{Kn}} [247 u_{ij}^{1(\alpha)} - 469 \sigma_{ij}^{(\alpha)}] \\ - \frac{\Omega}{\text{Kn}} [\delta_{18} u_{ij}^{1(\alpha)} - \delta_{19} \sigma_{ij}^{(\alpha)} - \delta_{20} u_{ij}^{1(\beta)} - \delta_{21} \sigma_{ij}^{(\beta)}], \end{aligned} \quad (14)$$

$$\begin{aligned} \sqrt{r_m} \frac{\partial \Delta_\alpha}{\partial t} + 8 \frac{\partial q_i^{(\alpha)}}{\partial x_i} - 20 \frac{\partial u_i^{(\alpha)}}{\partial x_i} = -\frac{2}{3} \frac{r_n r_d^2}{\text{Kn}} \Delta_\alpha \\ - \frac{\Omega}{\text{Kn}} [\delta_{22} \Delta_\alpha - \delta_{23} \Delta_\beta + \delta_{24} (T_\alpha - T_\beta)], \end{aligned} \quad (15)$$

where  $r_n = n_\alpha^\circ / n_\beta^\circ$ ,  $r_m = m_\alpha / m_\beta$  and  $r_d = d_\alpha / d_\beta$  are the ratio of ground state number densities, the ratio of masses and the ratio of diameters, respectively;  $\text{Kn} =$

$5/(16\sqrt{\pi}n_\beta^\circ d_\beta^2 L)$  is the Knudsen number for  $\beta$ -constituent; and  $\Omega = (1 + r_d)^2$ . Further,  $\delta_i$ 's in (9)–(15) depend only on the masses of the gas molecules through the relation  $\delta_i = \bar{\delta}_i \sqrt{2\mu_\beta}$  for all  $i$ , where  $\mu_\gamma = m_\gamma/(m_\alpha + m_\beta)$  for  $\gamma \in \{\alpha, \beta\}$  are the mass ratios [20] and

$$\begin{aligned}\bar{\delta}_1 &= \frac{5(1 + \mu_\alpha)}{48}, \quad \bar{\delta}_2 = \frac{\mu_\beta}{24}, \quad \bar{\delta}_3 = \frac{5(1 + \mu_\beta)\sqrt{r_m}}{48} \\ \bar{\delta}_4 &= \frac{\mu_\alpha\sqrt{r_m}}{24}, \quad \bar{\delta}_5 = \frac{5\mu_\alpha}{8}, \quad \bar{\delta}_6 = \frac{\mu_\alpha\mu_\beta}{48}, \\ \bar{\delta}_7 &= \frac{\mu_\alpha^2}{48}, \quad \bar{\delta}_8 = \frac{3 + 3\mu_\alpha + 4\mu_\alpha^2}{24}, \\ \bar{\delta}_9 &= \frac{\mu_\beta(3 + 4\mu_\alpha)}{168}, \quad \bar{\delta}_{10} = 8\bar{\delta}_6, \quad \bar{\delta}_{11} = \frac{8\bar{\delta}_7}{7}, \\ \bar{\delta}_{12} &= \frac{6 - 5\mu_\alpha + 9\mu_\alpha^2}{16}, \\ \bar{\delta}_{13} &= \frac{5(6 - 13\mu_\alpha + 27\mu_\alpha^2)}{96}, \\ \bar{\delta}_{14} &= \frac{\bar{\delta}_4(5 + 27\mu_\beta)}{2}, \\ \bar{\delta}_{15} &= \frac{5(12 - 34\mu_\alpha + 27\mu_\alpha^2)\sqrt{r_m}}{96}, \\ \bar{\delta}_{16} &= \frac{16 + 10\mu_\alpha + 9\mu_\alpha^2}{56}, \\ \bar{\delta}_{17} &= \frac{9\mu_\alpha\mu_\beta\sqrt{r_m}}{56}, \\ \bar{\delta}_{18} &= \frac{72 + 39\mu_\alpha - 91\mu_\alpha^2 + 120\mu_\alpha^3}{168}, \\ \bar{\delta}_{19} &= \frac{24 + 9\mu_\alpha - 83\mu_\alpha^2 + 120\mu_\alpha^3}{24}, \\ \bar{\delta}_{20} &= \frac{\mu_\alpha^2(7 + 30\mu_\beta)}{42}, \quad \bar{\delta}_{21} = \frac{\mu_\alpha\mu_\beta(9 - 30\mu_\alpha)}{6}, \\ \bar{\delta}_{22} &= \frac{\mu_\alpha(13 - 18\mu_\alpha + 15\mu_\alpha^2)}{12}, \quad \bar{\delta}_{23} = \frac{5\mu_\alpha^2\mu_\beta}{4}, \\ \bar{\delta}_{24} &= 120\bar{\delta}_6.\end{aligned}$$

The linear-dimensionless G26 equations for the  $\beta$ -constituent follow by setting  $r_m = 1$ , replacing  $r_n r_d^2$  by 1 and  $\Omega$  by  $r_n \Omega$ , and interchanging  $\alpha$  and  $\beta$  on both sides of (8)–(15). The dimensionless momentum balance equation for the mixture reads

$$\begin{aligned}\frac{\partial v_i}{\partial t} &= -\frac{r_n}{r_m r_n + 1} \left( \frac{\partial n_\alpha}{\partial x_i} + \frac{\partial T_\alpha}{\partial x_i} + \frac{\partial \sigma_{ij}^{(\alpha)}}{\partial x_j} \right) \\ &\quad - \frac{1}{r_m r_n + 1} \left( \frac{\partial n_\beta}{\partial x_i} + \frac{\partial T_\beta}{\partial x_i} + \frac{\partial \sigma_{ij}^{(\beta)}}{\partial x_j} \right). \quad (16)\end{aligned}$$

Thus, we shall have total  $(2 \times 26 + 1)$  equations in three dimensions and we shall simply ignore the equation for diffusion velocity of  $\beta$ -constituent because of the aforementioned reason.

## 4. Dispersion Relation

In this section, we discuss the behaviour of linear waves predicted by  $2 \times G26$  equations for hard sphere gases. In order to verify the linear stability of  $2 \times G26$  equations, we consider them in one dimension (1D). For  $\alpha$ -constituent, they read

$$\sqrt{r_m} \left( \frac{dn_\alpha}{dt} + \frac{dv_x}{dx} \right) + \frac{du_x^{(\alpha)}}{dx} = 0, \quad (17)$$

$$\begin{aligned}\sqrt{r_m} \frac{du_x^{(\alpha)}}{dt} + r_m \frac{dv_x}{dt} + \frac{d\sigma_{xx}^{(\alpha)}}{dx} + \frac{dn_\alpha}{dx} + \frac{dT_\alpha}{dx} \\ = -\frac{\Omega}{\text{Kn}} [\delta_1 u_x^{(\alpha)} + \delta_2 q_x^{(\alpha)} - \delta_3 u_x^{(\beta)} - \delta_4 q_x^{(\beta)}], \quad (18)\end{aligned}$$

$$\begin{aligned}\sqrt{r_m} \left( \frac{3}{2} \frac{dT_\alpha}{dt} + \frac{dv_x}{dx} \right) - \frac{3}{2} \frac{du_x^{(\alpha)}}{dx} + \frac{dq_x^{(\alpha)}}{dx} \\ = -\frac{\Omega}{\text{Kn}} [\delta_5 (T_\alpha - T_\beta) + \delta_6 \Delta_\alpha - \delta_7 \Delta_\beta], \quad (19)\end{aligned}$$

$$\begin{aligned}\sqrt{r_m} \left( \frac{d\sigma_{xx}^{(\alpha)}}{dt} + \frac{4}{3} \frac{dv_x}{dx} \right) + \frac{dm_{xxx}^{(\alpha)}}{dx} + \frac{8}{15} \frac{dq_x^{(\alpha)}}{dx} \\ = -\frac{1}{28} \frac{r_n r_d^2}{\text{Kn}} [21\sigma_{xx}^{(\alpha)} + u_{xx}^{1(\alpha)}] \\ - \frac{\Omega}{\text{Kn}} [\delta_8 \sigma_{xx}^{(\alpha)} + \delta_9 u_{xx}^{1(\alpha)} - \delta_{10} \sigma_{xx}^{(\beta)} - \delta_{11} u_{xx}^{1(\beta)}], \quad (20)\end{aligned}$$

$$\begin{aligned}\sqrt{r_m} \frac{dq_x^{(\alpha)}}{dt} + \frac{5}{2} r_m \frac{dv_x}{dt} + \frac{1}{2} \frac{du_{xx}^{1(\alpha)}}{dx} + \frac{1}{6} \frac{d\Delta_\alpha}{dx} \\ + \frac{5}{2} \frac{dn_\alpha}{dx} + 5 \frac{dT_\alpha}{dx} = -\frac{1}{3} \frac{r_n r_d^2}{\text{Kn}} [2q_x^{(\alpha)} - 5u_x^{(\alpha)}] \\ - \frac{\Omega}{\text{Kn}} [\delta_{12} q_x^{(\alpha)} - \delta_{13} u_x^{(\alpha)} - \delta_{14} q_x^{(\beta)} - \delta_{15} u_x^{(\beta)}], \quad (21)\end{aligned}$$

$$\begin{aligned}\sqrt{r_m} \frac{dm_{xxx}^{(\alpha)}}{dt} + \frac{9}{35} \frac{du_{xx}^{1(\alpha)}}{dx} = -\frac{3}{2} \frac{r_n r_d^2}{\text{Kn}} m_{xxx}^{(\alpha)} \\ - \frac{\Omega}{\text{Kn}} [\delta_{16} m_{xxx}^{(\alpha)} - \delta_{17} m_{xxx}^{(\beta)}], \quad (22)\end{aligned}$$

$$\begin{aligned} & \sqrt{r_m} \left( \frac{du_{xx}^{1(\alpha)}}{dt} + \frac{28}{3} \frac{dv_x}{dx} \right) + 9 \frac{dm_{xxx}^{(\alpha)}}{dx} + \frac{112}{15} \frac{dq_x^{(\alpha)}}{dx} \\ & - \frac{28}{3} \frac{du_x^{(\alpha)}}{dx} = -\frac{1}{168} \frac{r_n r_d^2}{\text{Kn}} [247u_{xx}^{1(\alpha)} - 469\sigma_{xx}^{(\alpha)}] \\ & - \frac{\Omega}{\text{Kn}} [\delta_{18}u_{xx}^{1(\alpha)} - \delta_{19}\sigma_{xx}^{(\alpha)} - \delta_{20}u_{xx}^{1(\beta)} - \delta_{21}\sigma_{xx}^{(\beta)}], \end{aligned} \quad (23)$$

$$\begin{aligned} & \sqrt{r_m} \frac{d\Delta_\alpha}{dt} + 8 \frac{dq_i^{(\alpha)}}{dx_i} - 20 \frac{du_i^{(\alpha)}}{dx_i} = -\frac{2}{3} \frac{r_n r_d^2}{\text{Kn}} \Delta_\alpha \\ & - \frac{\Omega}{\text{Kn}} [\delta_{22}\Delta_\alpha - \delta_{23}\Delta_\beta + \delta_{24}(T_\alpha - T_\beta)]. \end{aligned} \quad (24)$$

The 1D equations for  $\beta$ -constituent can be written in a similar way. The momentum balance equation for the mixture (16) in 1D reads

$$\begin{aligned} \frac{dv_x}{dt} = & -\frac{r_n}{r_m r_n + 1} \left( \frac{dn_\alpha}{dx} + \frac{dT_\alpha}{dx} + \frac{d\sigma_{xx}^{(\alpha)}}{dx} \right) \\ & - \frac{1}{r_m r_n + 1} \left( \frac{dn_\beta}{dx} + \frac{dT_\beta}{dx} + \frac{d\sigma_{xx}^{(\beta)}}{dx} \right). \end{aligned} \quad (25)$$

For the field variables

$$\begin{aligned} \mathbf{U} = \{ & n_\alpha, u_x^{(\alpha)}, T_\alpha, \sigma_{xx}^{(\alpha)}, q_x^{(\alpha)}, m_{xxx}^{(\alpha)}, u_{xx}^{1(\alpha)}, \Delta_\alpha, \\ & n_\beta, T_\beta, \sigma_{xx}^{(\beta)}, q_x^{(\beta)}, m_{xxx}^{(\beta)}, u_{xx}^{1(\beta)}, \Delta_\beta, v_x \}^\top, \end{aligned}$$

we consider the plane wave ansatz

$$\mathbf{U} = \mathbf{U}_A \exp \{i(x - \hat{\omega}t)\}, \quad (26)$$

where we have assumed that the length scale  $L$  is the inverse of the wave number  $\kappa$ ,  $\hat{\omega} = \omega/(\kappa v_0)$  is the dimensionless complex frequency of the wave with  $\omega$  as the conventional complex frequency and  $\mathbf{U}_A$  is the vector consisting of complex amplitudes. In this case, the Knudsen number  $\text{Kn} = (5\kappa)/(16\sqrt{\pi}n_\beta^\circ d_\beta^2)$  takes the role of a dimensionless wave number. Substitution of the ansatz (26) into the above 1D moment equations yields an algebraic equation  $\mathcal{A}(\hat{\omega}, \mu_\alpha, r_d, r_n, \text{Kn}) \mathbf{U} = \mathbf{0}$ . For non-trivial solutions  $\mathbf{U}$ , the determinant of matrix  $\mathcal{A}$  should vanish, i.e.,  $\det \mathcal{A} = 0$ . The condition  $\det \mathcal{A} = 0$  gives the so-called dispersion relation relating  $\hat{\omega}$  and dimensionless wave number  $\text{Kn}$  (here).

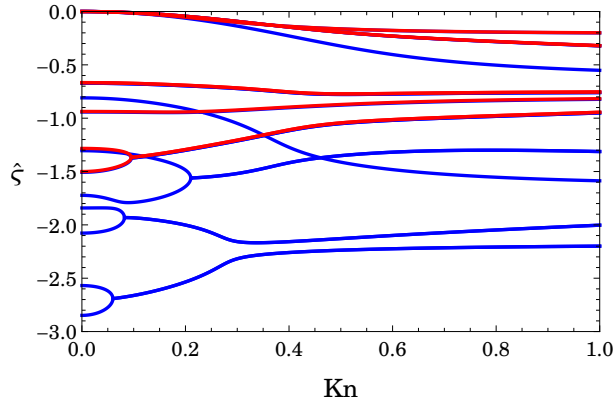
## 4.1 Temporal Stability

For temporal stability, the wave number  $\kappa$  is assumed to be real whereas the frequency  $\omega$  is assumed to be complex. The associated wave travels with phase velocity  $v_{\text{ph}} = \text{Re}(\omega)/\kappa$  and the growth rate of the amplitudes is characterised by the damping coefficient  $\varsigma = \text{Im}(\omega)$ . Temporal stability requires  $\varsigma \leq 0$ .

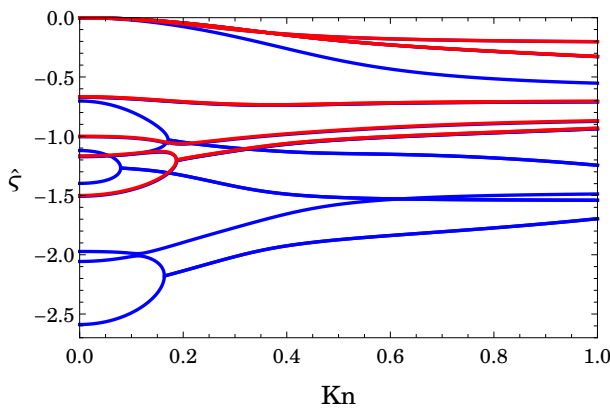
## 5. Results

In order to illustrate the linear stability, we plot the dimensionless damping coefficient  $\hat{\varsigma} = (5\varsigma)/(16\sqrt{\pi}n_\beta^\circ d_\beta^2 v_0)$  over the Knudsen number  $\text{Kn}$  for parameters  $\mu_\alpha = 0.3$ ,  $r_n = 0.005$  in figure 1. Figures 1(a) and 1(b) show the damping coefficients of all the modes of the  $2 \times \text{G26}$  equations for hard spheres and Maxwell molecules, respectively; for hard spheres the diameter ratio  $r_d$  is taken as 1 and for Maxwell molecules the ratios of all collision cross sections are taken as 1. The equations for Maxwell molecules can be found in [10]. The red curves in figure 1 show the modes for single gas by considering  $r_n = 0$  while the blue curves show the modes for binary gas-mixture. The red curves are included only for comparison. Clearly, for all the modes damping is non-positive. Moreover, for all permissible values of the parameters, damping remains non-positive for both hard spheres and Maxwell molecules. Therefore, we conclude empirically that the  $2 \times \text{G26}$  equations for hard spheres as well as Maxwell molecules are linearly stable.

To have more insight into the dispersion modes in figure 1, we plot the dimensionless damping  $\hat{\varsigma}$  over the dimensionless phase velocity  $\hat{v}_{\text{ph}}$  for (a) hard spheres and (b) Maxwell molecules in figure 2. The Knudsen number in figure 2 varies between 0 and 20, and the other parameters are same as those in figure 1. Again, the red curves represent the modes for single gas whereas the blue curves represent the modes for binary gas-mixture, and the black dots depict the start-



(a) Hard spheres



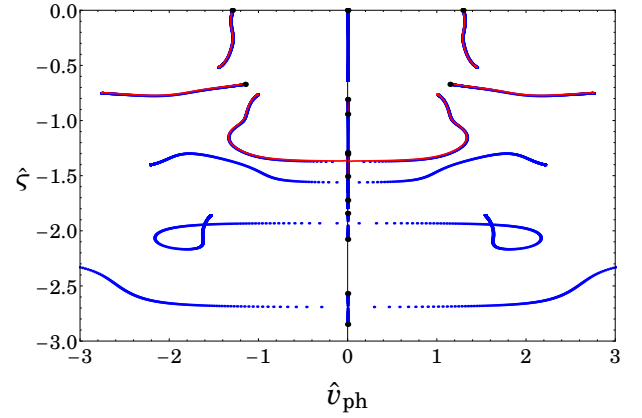
(b) Maxwell molecules

Figure 1: Damping coefficients  $\hat{\zeta}$  of all the modes of  $2 \times G26$  equations for (a) hard spheres and (b) Maxwell molecules plotted over the Knudsen number  $Kn$ .

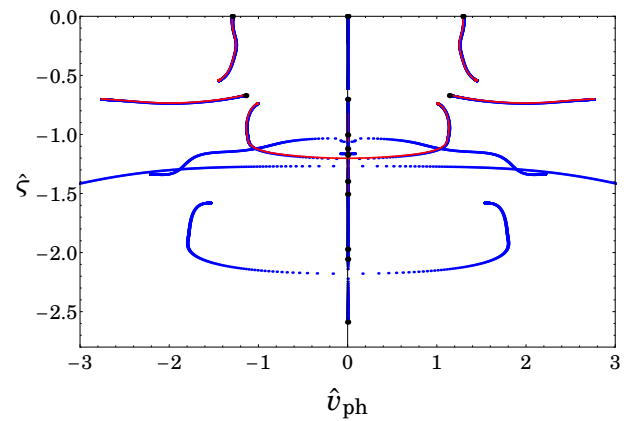
ing point of the modes at  $Kn = \kappa = 0$ . At  $Kn = \kappa = 0$ , four sound modes commence with non-zero velocities, two of them have zero damping and other two have non-zero damping at the start. One sound mode begins with zero damping and zero velocity. All other modes are pure diffusion modes which start with zero velocity and have non-zero damping. Some of the diffusion modes (8 in each figure) bifurcate into propagating waves with damping.

## 6. Conclusion

In this paper, the derivation of fully non-linear  $2 \times G26$  equations for a binary gas-mixture of monatomic-inert-ideal hard



(a) Hard spheres



(b) Maxwell molecules

Figure 2: Damping coefficients  $\hat{\zeta}$  of all the modes of  $2 \times G26$  equations for (a) hard spheres and (b) Maxwell molecules plotted over the phase velocity  $\hat{v}_{ph}$  for  $0 \leq Kn \leq 20$ .

sphere gases has been outlined, though—for brevity—the full non-linear  $2 \times G26$  equations have not been shown and only the linear  $2 \times G26$  equations are presented. In order to obtain the dispersion relation for stability analysis, the linear  $2 \times G26$  equations have been restricted to 1D. Assuming the plane wave solution, it has been concluded empirically as well as with the plots for some parameter values that the  $2 \times G26$  equations for binary mixture of hard sphere gases are linearly stable.

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